



ISPRAS OPEN Moscow 2019

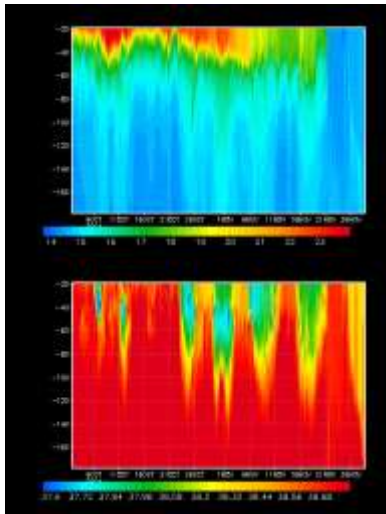
## Identification of turbulent model parameters in ocean surface models

*Turboradar / Turbident / Urbarisq*

C. Aldebert, M. Baklouti, D. Bourras, H. Branger, T. Caby, J.L. Devenon, D. Faranda, P. Fraunié, R. Fuchs, P. Garreau, G. Koenig, I. Pairaud, V. Rey, A. Sentchev, V. Shrira, S. Vaienti



# Surface layer problem



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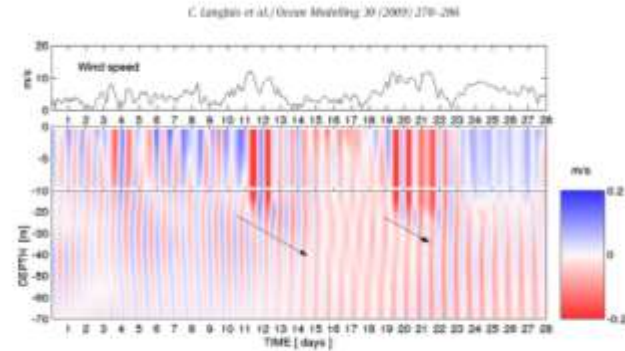


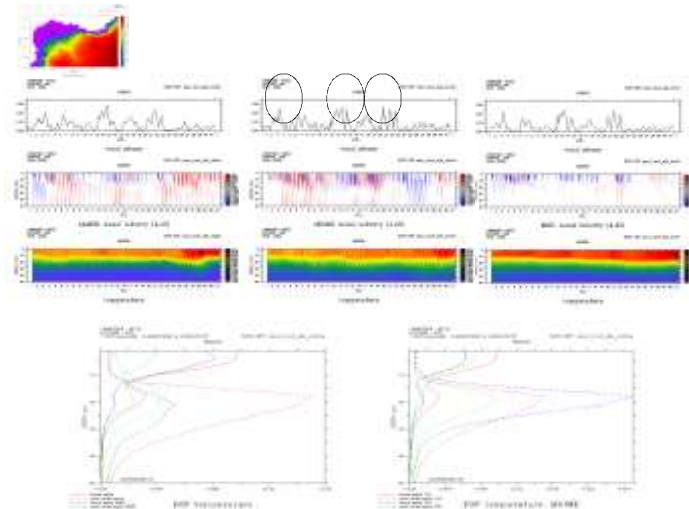
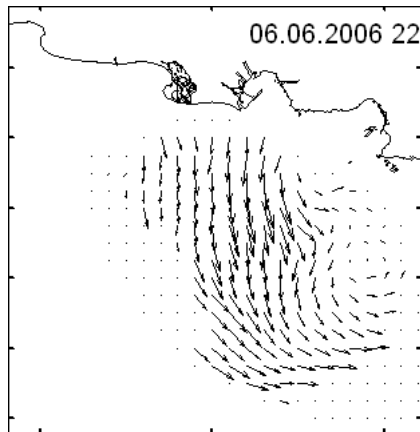
Fig. 18. Time evolution of the wind speed and of the vertical profile of the zonal current at 3.1°E, 42.0°N during a 28 day period in summer, in a simulation with the GCM ocean circulation model driven with ERA40 forcing.

## Internal waves permitting models: summer 2008

Langlais et al, 2009, Schaeffer et al 2010

## Gliders observations

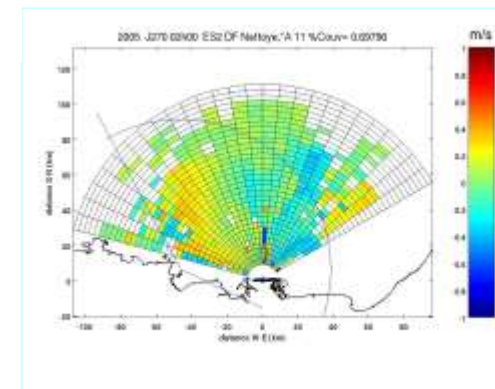
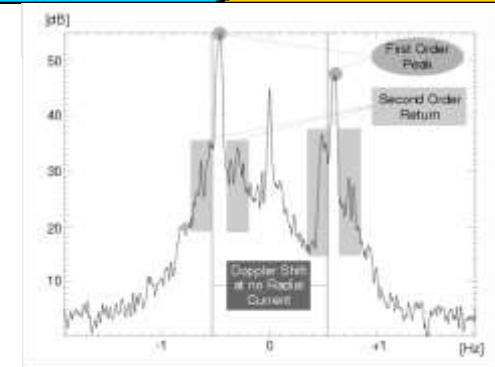
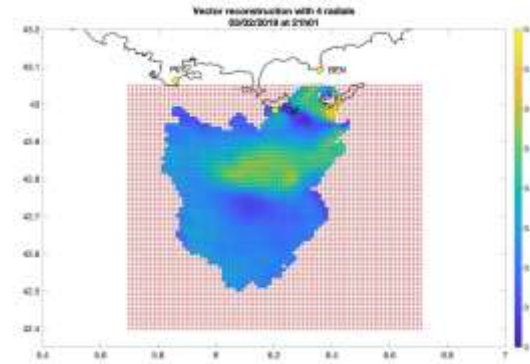
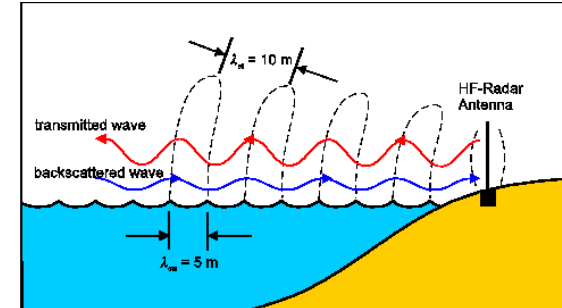
(Testor et al, 2008)



## HF radars observations

(Forget & Shrira, 2015)

# HF radars H current mapping

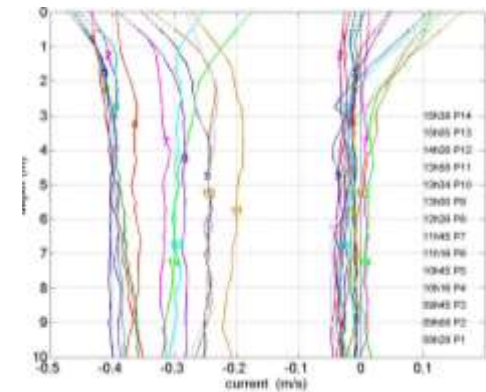
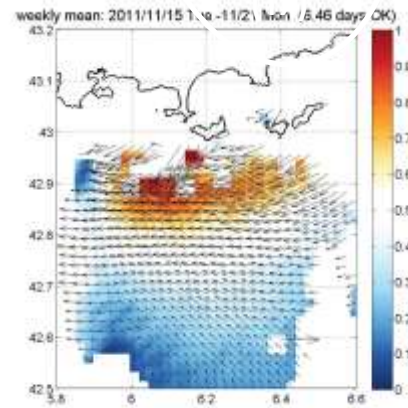
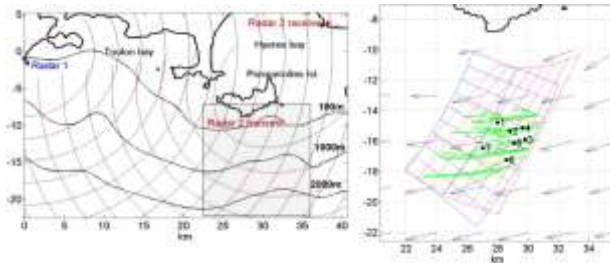


**M.I.O. HF Radar team :** C. A. Guérin (PR), C. Quentin(IR),  
A. Gramoullé (IE), D. Dumas(IE), B. Zakardjian(PR), A. Molcard (PR),  
M. Saillard (PR)

**MOOSE / EU MARITTIMO SICOMAR PLUS / ANR TURBIDENT**

# SUBCORAD campaign 2013

Sentchev, Forget, Fraunié, 2015



# The Ekman (1905) solution

$$\frac{\partial u}{\partial t} - fv = \nu_t \frac{\partial^2 u}{\partial z^2}$$

$$\frac{\partial v}{\partial t} + fu = \nu_t \frac{\partial^2 v}{\partial z^2}$$

- Steady solution

$$\begin{cases} U(z) = \text{sign}(f) U_c \sqrt{2} \exp\left(-\frac{z}{d_E}\right) \cos\left(\frac{\pi}{4} - \frac{z}{d_E}\right) \\ V(z) = U_c \sqrt{2} \exp\left(-\frac{z}{d_E}\right) \sin\left(\frac{\pi}{4} - \frac{z}{d_E}\right) \end{cases}$$

- unsteady solution

$$\begin{cases} U(z,t) = \frac{2 \tau_{xy}}{\rho_f d_E f} \int_0^{\bar{t}} \frac{\sin(2 \pi \zeta)}{\sqrt{\zeta}} \exp\left(-\frac{z^2}{4 \pi d_E^2 \zeta}\right) d\zeta \\ V(z,t) = \frac{2 \tau_{xy}}{\rho_f d_E |f|} \int_0^{\bar{t}} \frac{\cos(2 \pi \zeta)}{\sqrt{\zeta}} \exp\left(-\frac{z^2}{4 \pi d_E^2 \zeta}\right) d\zeta \end{cases}$$

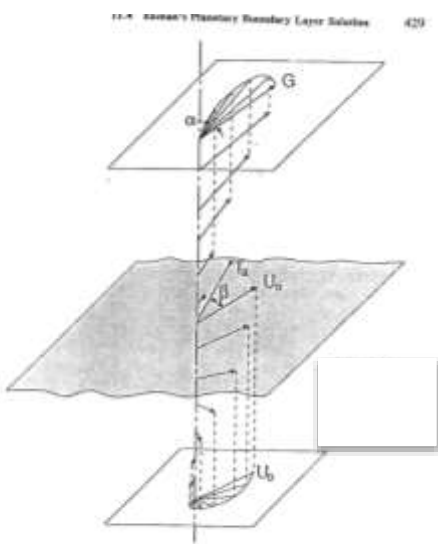


Figure 11.6 Sketch of velocity vectors in the surface atmospheric and oceanic PBLs. Note the change in rotation.

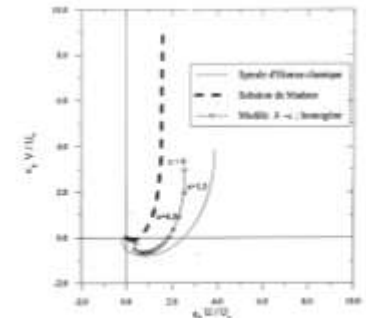
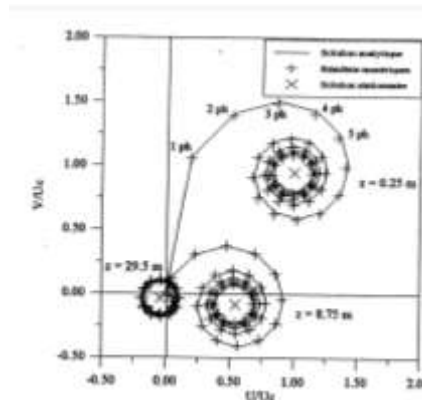
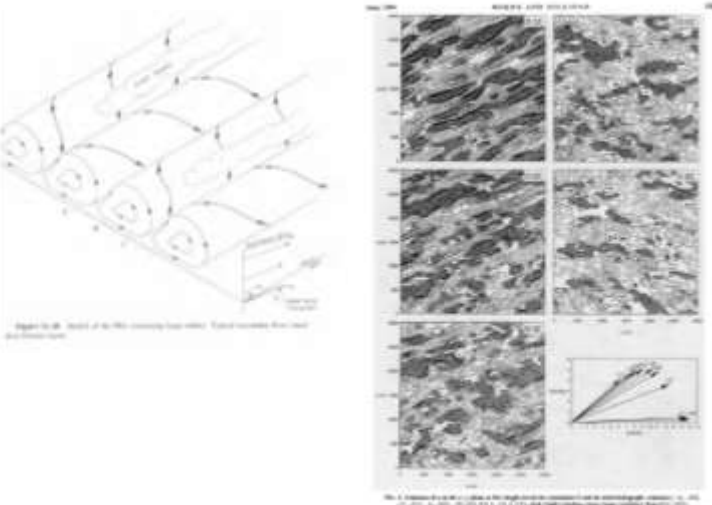


Fig. 11.7 A Ekman layer, evolution en fonction de la profondeur du vecteur vitesse obtenu avec le modèle 11-6, chaque point représente le vecteur vitesse à une profondeur z (m) indiquée sur les premiers points.

K-ε model (C. Verdier-Bonnet 1996, 1999)

# Ekman layer inflectional Instability

- Ekman Spiral (Ekman 1905, Gonella 1971, Madsen 1977, Lewis&Belcher 2004, Elipot&Gille 2009, Almelah&Shrira sub)
- Stability analysis (Faller 1965, Brown 1974, Leibovich & Lele, 1985)
- LES (Deardorff 1970, 1972, Mason & Thomson 1987, Moeng&Sullivan 1994, Zikanov et al, 2003, Sullivan&McWilliams 2010)
- DNS (Coleman, Ferziger, Spalart, 1990)
- Observations PBL (Le Mone 1973)
- Observations Ocean (Price et al 1987, 1999, Csanady 2001)



Moeng&Sullivan 1994

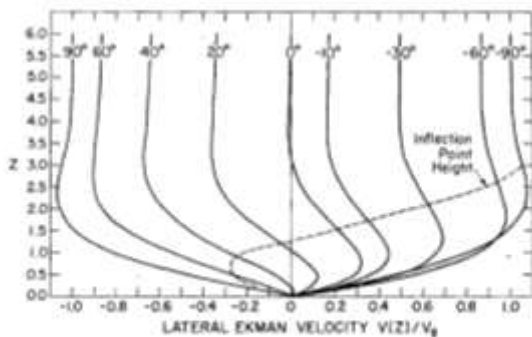


FIG. 1. Two-dimensional velocity profiles taken in vertical planes normal to the roll direction. The angle  $\alpha$  denotes the roll angle to the left of the geostrophic velocity. The height and velocity are given in increments of  $\delta$  and  $V_0$ , respectively.

Brown 1972

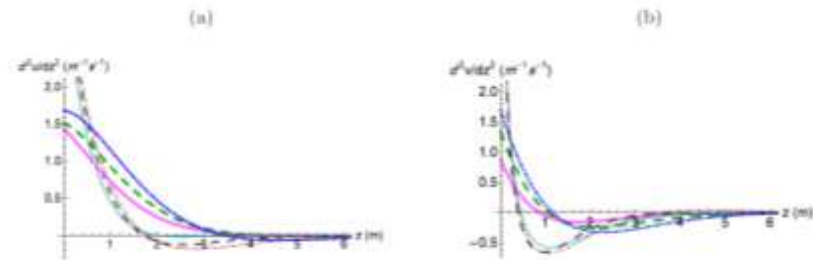
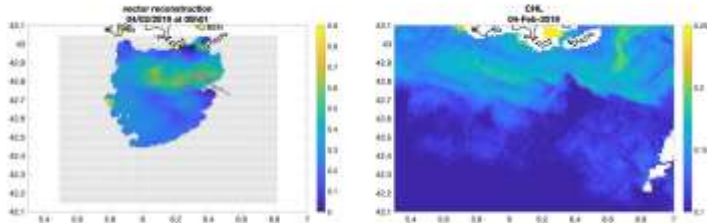


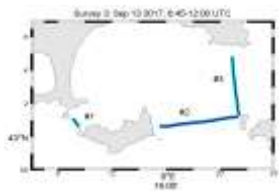
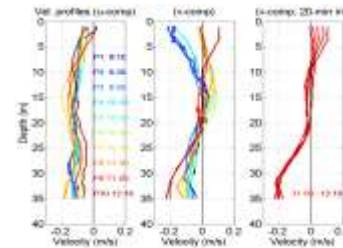
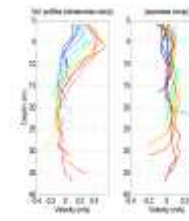
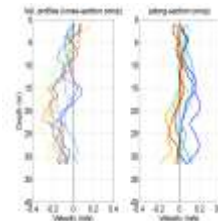
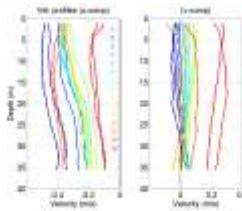
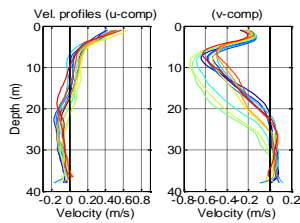
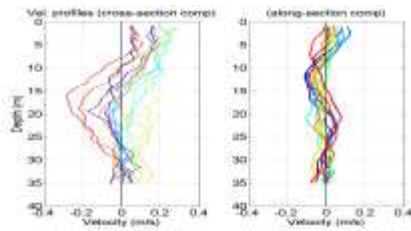
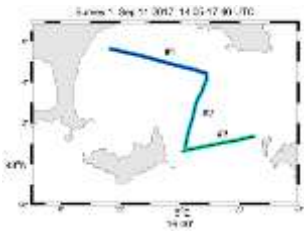
FIGURE 6. Second derivatives of the velocity profiles in two models of viscosity (the classical Ekman model (thick lines) and time-dependent viscosity model (thin lines)) at different times:  $\tilde{t} = 2$  (solid lines),  $\tilde{t} = 3$  (dashed lines) and  $\tilde{t} = 5$  (dotted lines). (a) The second derivative of  $x$ -component. (b) The second derivative of  $y$ -component. The parameters:  $\delta = 3$  hrs,  $f = 10^{-2} s^{-1}$ ,  $v_0 = 10^{-4} m^2 s^{-1}$ .

Almelah & Shrira sub

# TURBIDENT campaign 2018



Dumas, Granoullé & Guérin



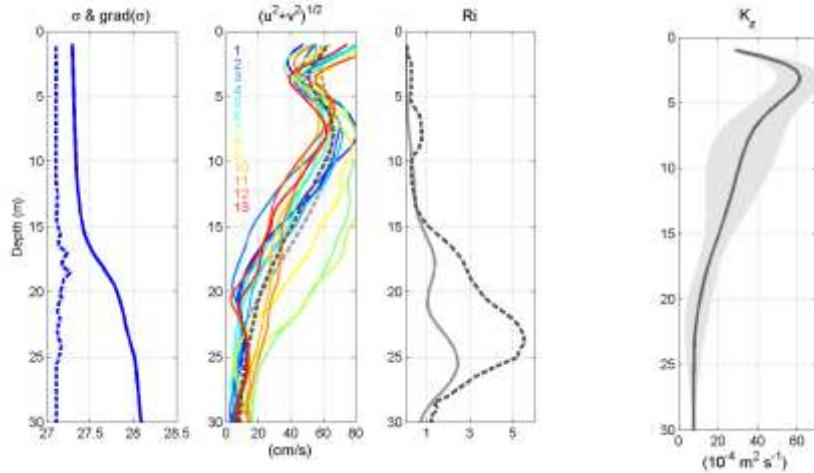
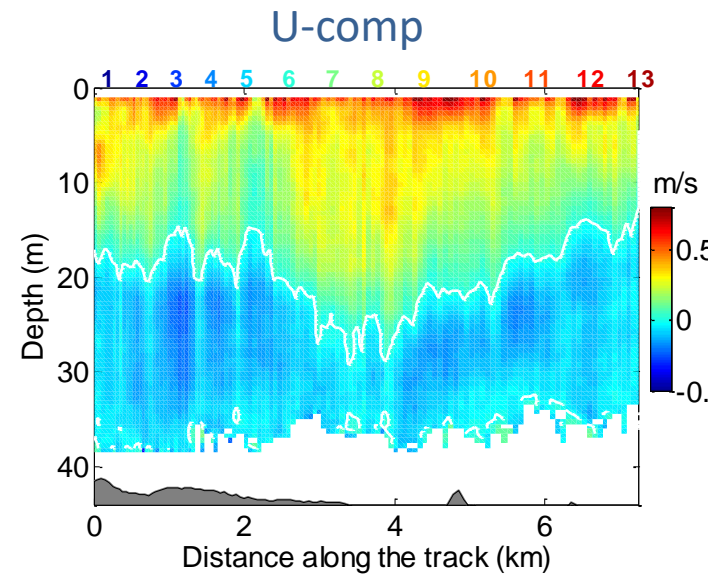
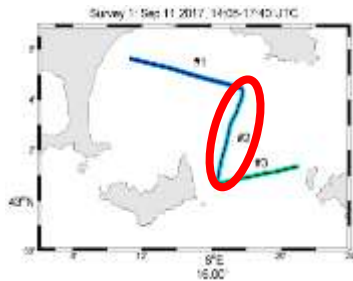
D. Bourras, H. Branger, A. Sentchev

**Table 1.** Overview of optimization methods, and their pros and cons when applied to complex geophysical models that are costly to program and run. We do not mention Kalman methods, which cannot be used for parameter identification in their current form (Sun et al., 2016).

Type	Method	Pros	Cons
By-hand		Easy, only model runs.	Need many runs, unlikely to succeed without a method.
Stochastic, global	Simulated-Annealing	Generic, easy to implement, noisy data.	Need many runs, even for a few parameters.
	Genetic algorithms	Generic, many parameters, noisy data.	Need many runs, hard to tune.
	Hamiltonian Monte-Carlo	Generic, Bayesian framework.	Need many runs
Local gradient descent	Adjoint	Cheap to run, explicit gradient, many parameters.	Costly to build, problem-specific, noise-sensitive.
	Finite-Difference	Generic, easy to implement, almost exact gradient.	Number of runs proportional to the number of parameters, noise-sensitive.
	Simultaneous Perturbation Stochastic Approximation	Generic, easy to implement, cheap to run, many parameters, less noise-sensitive.	Approximative gradient.



# Eddy viscosity estimate



From 1 D Ekman model (A Sentchev)

# Parameter estimation of turbulent closure schemes in marine circulation models using Simultaneous Perturbation Stochastic Approximation method : a proof-of-concept.

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(1) Mediterranean Institute of Oceanography, Aix-Marseille University, Toulon University, CNRS/IRD, France, (2) IFREMER Lérpar, La Seyne, France, (3) IFREMER LPOS, Brest, France

### The operational problem

- predictions by numerical models of marine circulation strongly rely on the description of the sea-air interface
- difficult to acquire reliable data close to sea surface  $\Rightarrow$  practical challenge is to parameterize the turbulent closure schemes modelling the upper mixing layer
- TURBIDENT project aims to optimize turbulent closure schemes with a new well-suited data set from HF radars and AUV-mounted ADCP
- we use a new data assimilation method that has never been used for turbulent closure schemes optimization

### Why this new method ?

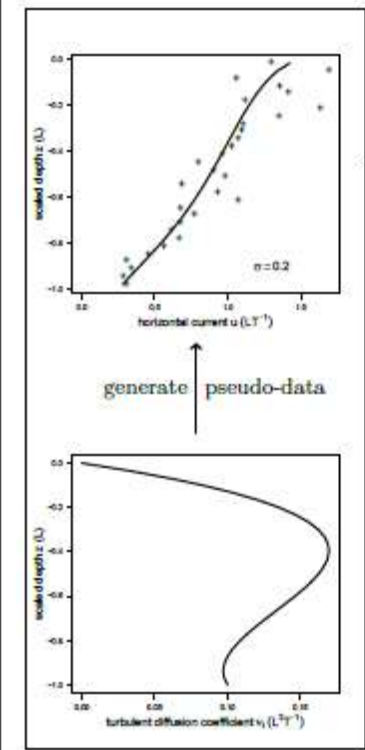
- model derivatives with respect to the parameters to optimize are usually computed explicitly by an adjoint model that need to be developed and maintained
- the SPSA methods (Zhu & Spall, 2002) are based on a small number of model estimates (random parameter perturbations) to approximate at low numerical cost the derivatives by finite differences
- due to the random component, different methods (first and second-order, "modified") has been proposed to improve the procedure (numerical cost, stability)

### Preliminary results

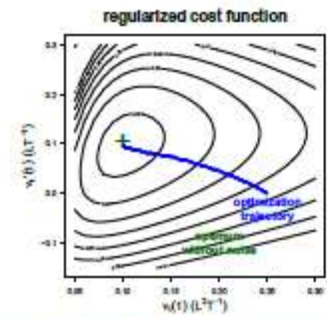
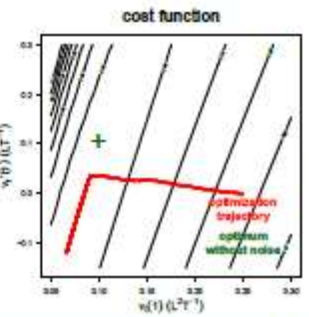
- we identified the most stable SPSA algorithm through theoretical examples of the surface layer
- ongoing tests for KPP model (link with interior domain, surface layer thickness)

### Next steps

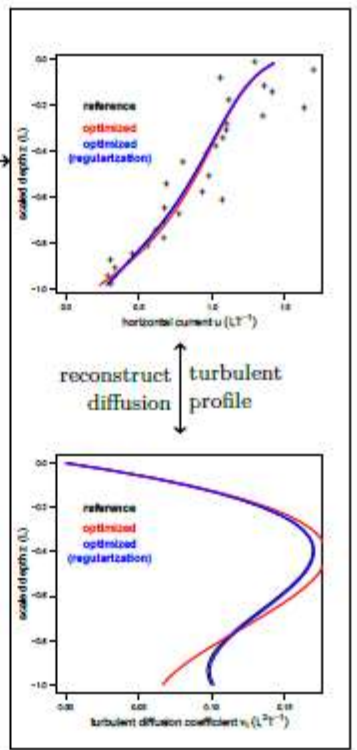
- stratified and/or unsteady situations
- sensitivity to sampling under realistic scenarios
- coupling SPSA with existing methods
- same work with k- $\epsilon$  model



data on current profile  
as constraints



optimize parameters  
to fit current profile



### A steady-state example

Horizontal current ( $u$ ) experiencing a turbulent diffusion (coefficient  $\nu_t$ ) along a scaled vertical axis ( $z \in [0, 1]$ ):

$$\frac{\partial}{\partial z} \left( \nu_t(z) \frac{\partial u}{\partial z} \right) = 0, \text{ with the boundary condition } u(0) = u_0$$

Like in KPP model (Large *et al.*, 1994),  $\nu_t(z)$  is taken as a third-order polynomial that depends on two parameters : its value  $\nu_t(1)$  and derivative  $\nu_t'(1)$  at the lower boundary (continuity with the interior profile in KPP model)

For reference parameters, we compute the  $\nu_t$  and  $u$  profiles. The current profile is sampled at depths  $z_i$  and a random noise is added to generate pseudo-data :

$$u_i^{obs} = \alpha_1 u(z_i), \alpha_1 \sim \mathcal{N}(1, \sigma)$$

### Outline of SPSA methods

For a set of parameters to optimize  $\theta$  (here  $\theta = (\nu_t(1), \nu_t'(1))$ ), we define a cost function, here :  $S(\theta) = \sum_{i=1}^n (u_i^{obs} - u_i^{mod}(\theta))^2 / n$ .

Starting from initial parameter values, each step involves :

1. simultaneous random perturbations :  $\Delta\theta_i = \pm 1$  (equiprobability)
2. use  $S(\theta \pm c\Delta\theta)$  to approximate the gradient by finite differences
3. optional : similar method for the Hessian (add 2 model runs)
4. use 2. and 3. to compute new parameter estimates (with checking)

For step 4., the modified SPSA method is the most stable :  $\theta^{new} = \theta - a \text{grad}(S(\theta))$ , where  $a$  is the mean of Hessian eigenvalues

One may include additional information in the cost function to regularize it, here (as example) :

$$S(\theta) = \sum_{i=1}^n (u_i^{obs} - u_i^{mod}(\theta))^2 / n + \lambda (\nu_t'(1) - \nu_t^{obs}(1))^2$$

# Classical standard values of TKE turbulent closure model parameters

**Table 2.** Model parameters. Gaspar et al. (1990)

Parameter	Value	Unit	Meaning
$c_k$	0.1	-	TKE constant (eddies diffusivity)
$c_\epsilon$	0.7	-	TKE constant (turbulent dissipation)
$K_{m_{\min}}$	$3 \cdot 10^{-5}$	$\text{m}^2 \cdot \text{s}^{-1}$	minimal value for moment diffusivity
$\bar{e}_{\min}$	$2 \cdot 10^{-6}$	$\text{m}^2 \cdot \text{s}^{-2}$	minimal value for TKE
$\bar{e}_{\min 0}$	$10^{-4}$	$\text{m}^2 \cdot \text{s}^{-2}$	minimal value for TKE at surface
$Pr_t$	1	-	Prandtl number
$K_{\text{ratio}}$	1	-	ratio between TKE and momentum diffusivities
$bb$	3.75	-	constant to compute surface TKE from wind stress

# Simple hydrodynamic model 1DV

- T temperature ; S salinity ;  $\mathbf{U}=(u,v)$  and w horizontal and vertical velocity , I solar irradiance,  $F_{\text{sol}}$  solar constant,  $c_p$  specific heat.

$$\frac{\partial \bar{T}}{\partial t} = \frac{F_{\text{sol}}}{\rho_0 c_p} \frac{\partial I}{\partial z} - \frac{\partial \overline{T'w'}}{\partial z},$$

$$\frac{\partial \bar{S}}{\partial t} = - \frac{\partial \overline{S'w'}}{\partial z},$$

$$\frac{\partial \mathbf{U}}{\partial t} = -f\mathbf{k} \times \mathbf{U} - \frac{\partial \overline{\mathbf{U}'w'}}{\partial z},$$

# Turbulent closure scheme

Eddy diffusivities:  $K_h$ ,  $K_s$ ,  $K_m$

$$\overline{T'w'} = -K_h \frac{\partial \bar{T}}{\partial z}, \quad \overline{S'w'} = -K_s \frac{\partial \bar{S}}{\partial z}, \quad \overline{U'w'} = -K_m \frac{\partial \bar{U}}{\partial z},$$

$$K_m = \max \left( K_{m_{\min}}, c_k l_k \sqrt{\bar{e}} \right),$$

$$K_s = K_h = \frac{K_m}{Pr_t},$$

# Turbulent closure scheme

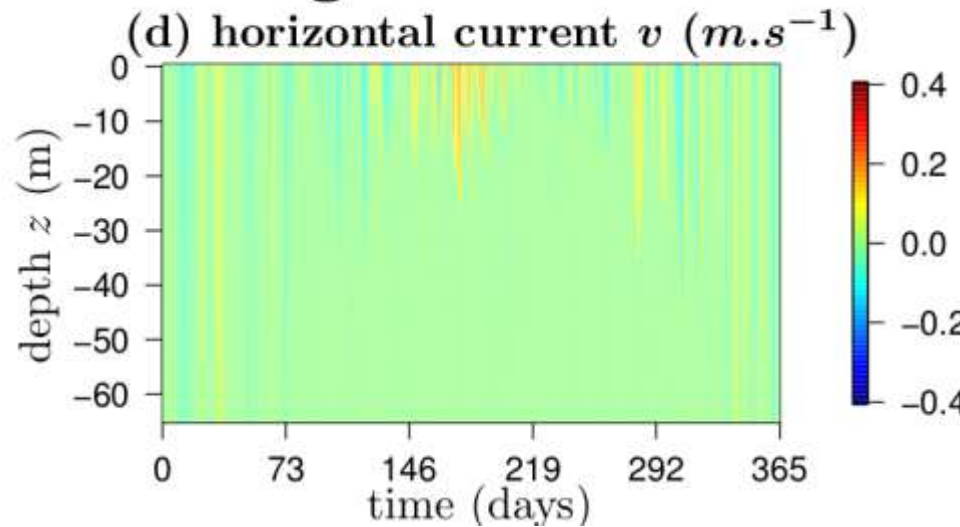
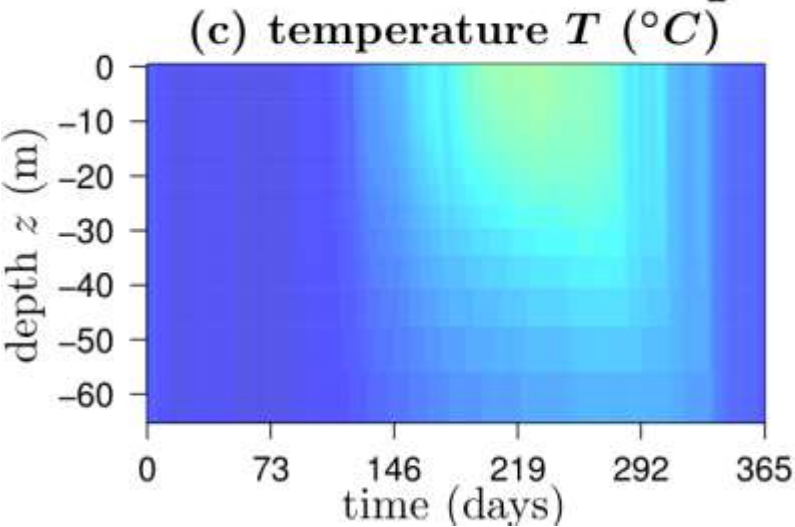
$$\bar{e} = 0.5(\overline{u'^2} + \overline{v'^2} + \overline{w'^2}) \quad \varepsilon = c_\varepsilon \frac{\bar{e}^{3/2}}{l_\varepsilon},$$

$$\frac{\partial \bar{e}}{\partial t} = \frac{\partial}{\partial z} \left( K_e \frac{\partial \bar{e}}{\partial z} \right) - \overline{\mathbf{U}'w'} \cdot \frac{\partial \mathbf{U}}{\partial z} + \overline{b'w'} - \varepsilon$$

$$\bar{e}_{(z=0)} = \max \left( \bar{e}_{\min 0}, bb \frac{\sqrt{\tau_x^2 + \tau_y^2}}{\rho} \right)$$

# Optimization : arbitrary starting state

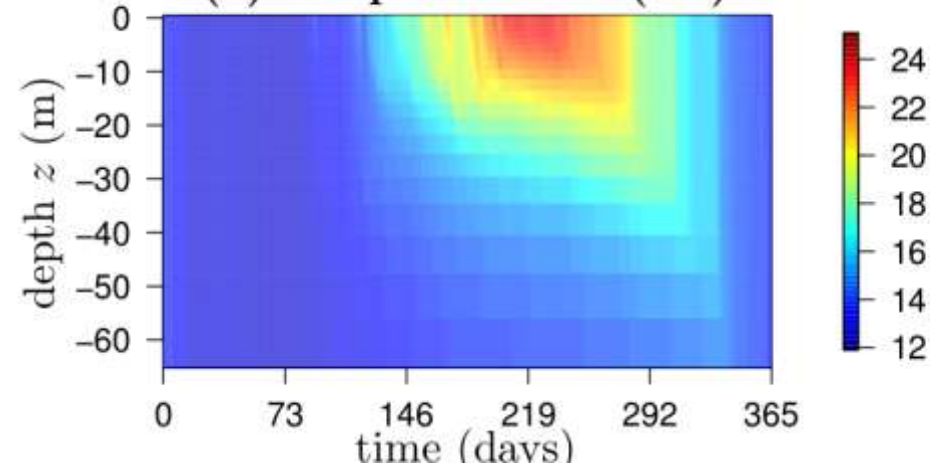
model prediction: first guess



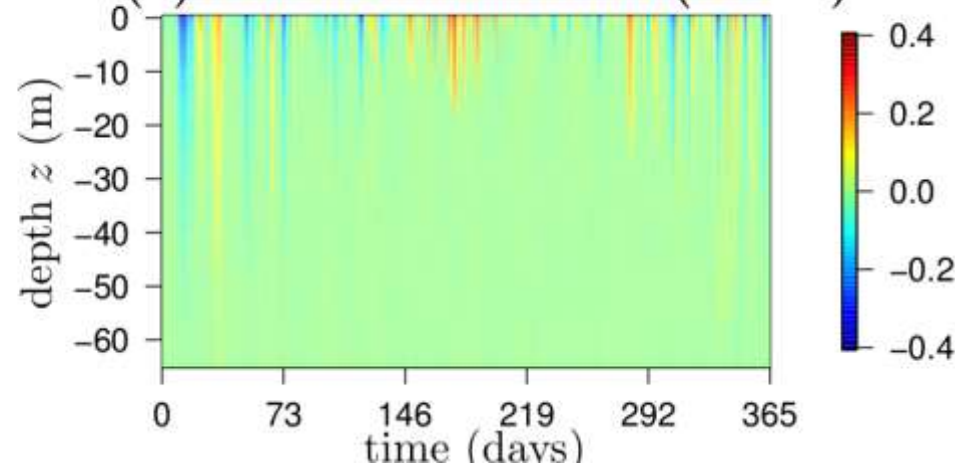
# Optimization : Twin experiments

available data

(a) temperature  $T$  ( $^{\circ}\text{C}$ )

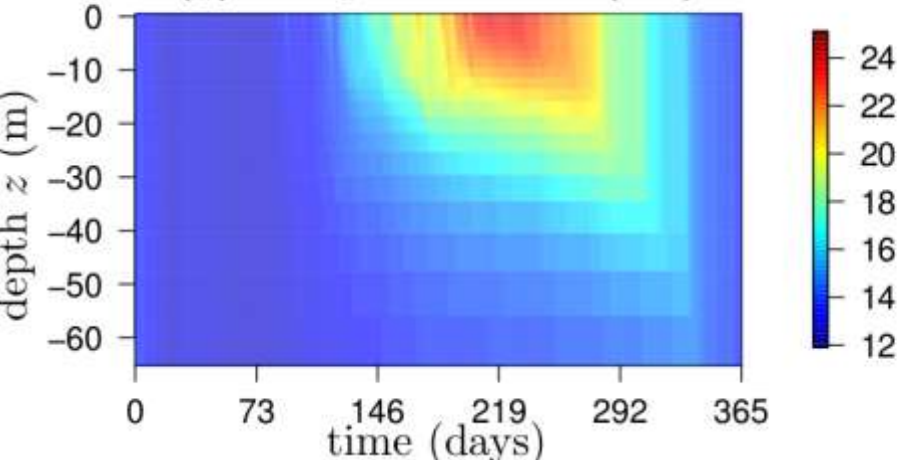


(b) horizontal current  $v$  ( $\text{m.s}^{-1}$ )

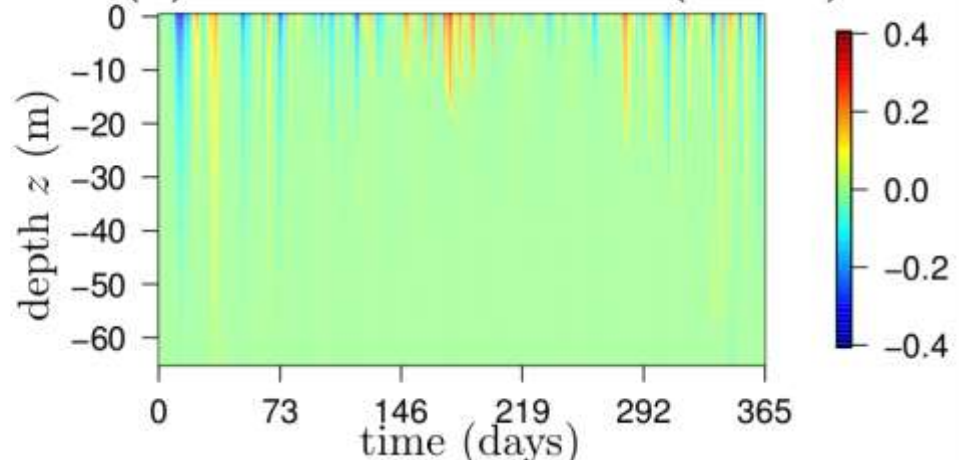


optimized prediction

(g) temperature  $T$  ( $^{\circ}\text{C}$ )



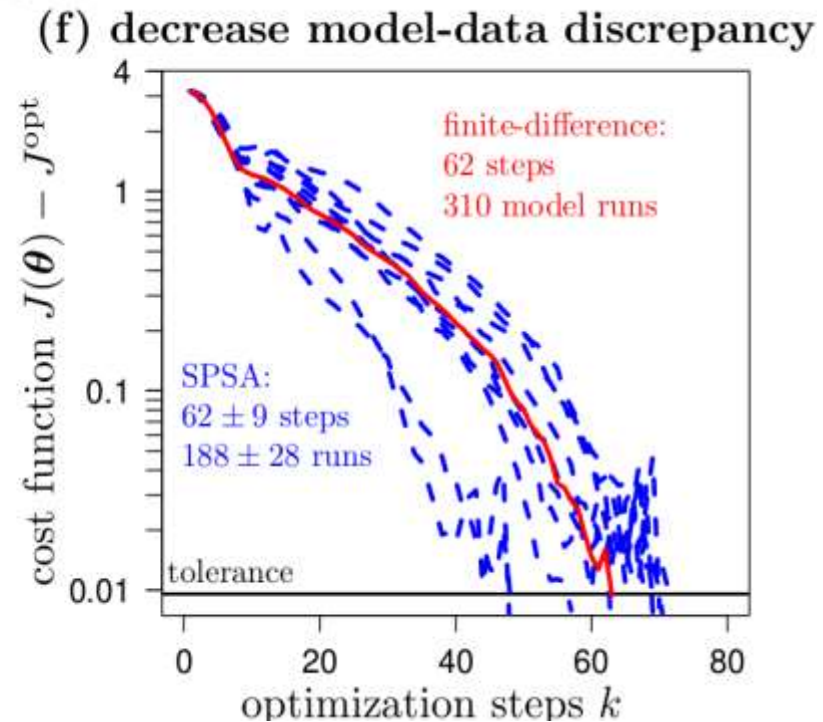
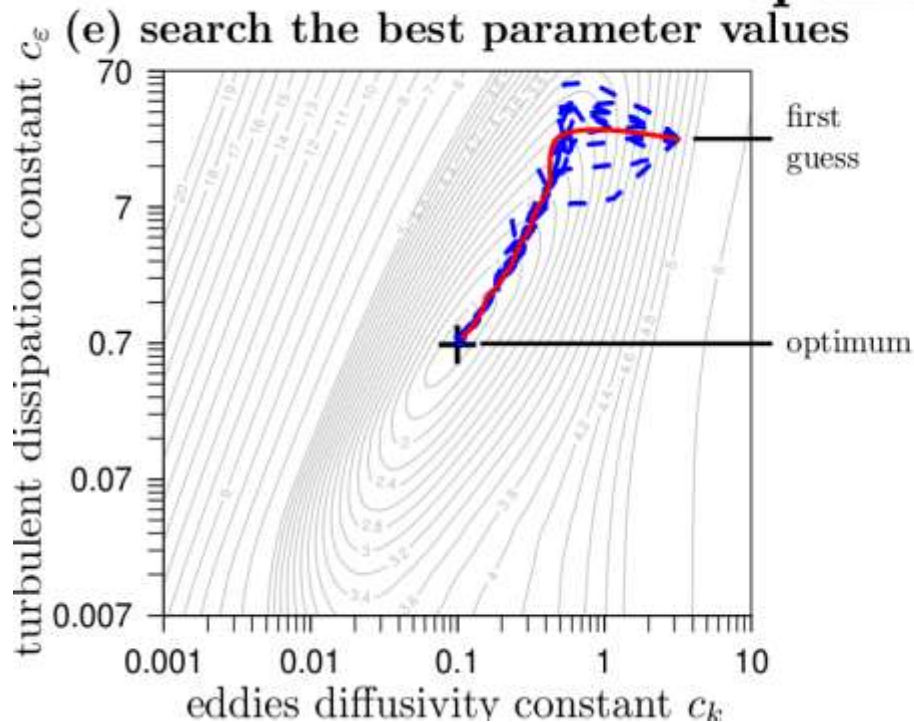
(h) horizontal current  $v$  ( $\text{m.s}^{-1}$ )





# Optimal search in the control space example in a 2D sub-space

## optimization



# Cost function and minimization algorithm

## (Nesterov Momentum)

$$J(\boldsymbol{\theta}) = \alpha_{uv} \left( \sum_{i=1}^n \left( u_i^{\text{pred}}(\boldsymbol{\theta}) - u_i^{\text{obs}} \right)^2 + \sum_{i=1}^n \left( v_i^{\text{pred}}(\boldsymbol{\theta}) - v_i^{\text{obs}} \right)^2 \right)^{1/2} \\ + \alpha_T \left( \sum_{i=1}^n \left( T_i^{\text{pred}}(\boldsymbol{\theta}) - T_i^{\text{obs}} \right)^2 \right)^{1/2} + \alpha_S \left( \sum_{i=1}^n \left( S_i^{\text{pred}}(\boldsymbol{\theta}) - S_i^{\text{obs}} \right)^2 \right)^{1/2},$$

procedure starting from an arbitrary initial guess of the parameter values  $\boldsymbol{\theta}^{(0)}$ :

$$\boldsymbol{\theta}^{(k+1)} = \boldsymbol{\theta}^{(k)} - a^{(k)} \mathbf{z}^{(k)}. \quad (2)$$

$a^{(k)}$  : step size       $\mathbf{z}^{(k)}$  searching direction

$$\mathbf{z}^{(k)} = \beta \mathbf{z}^{(k-1)} + \nabla J(\boldsymbol{\theta}^{(k)} - a^{(k)} \mathbf{z}^{(k-1)}).$$

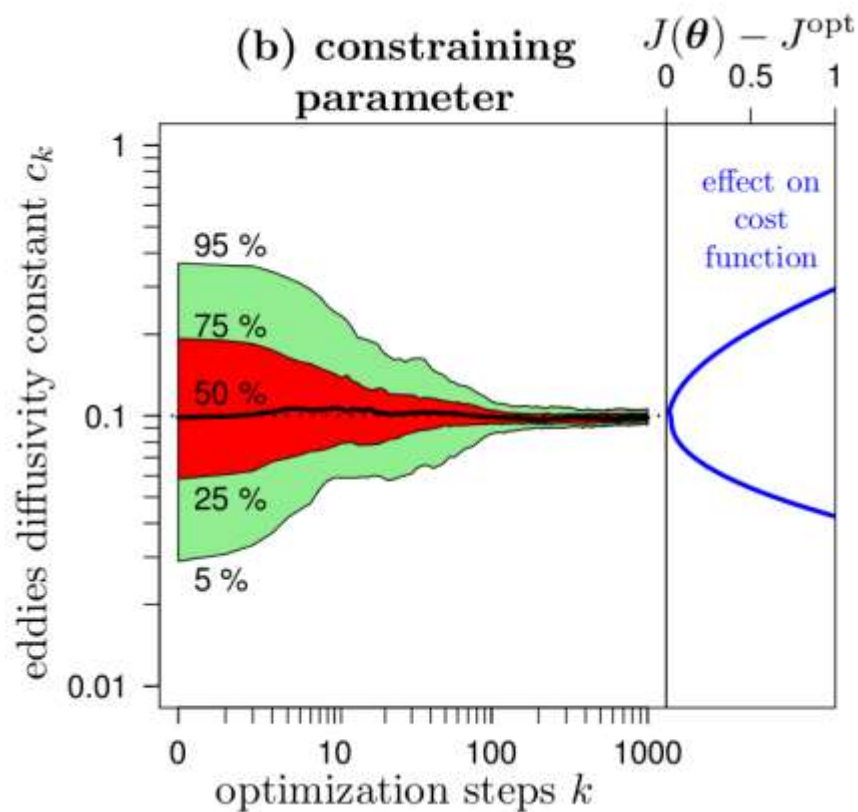
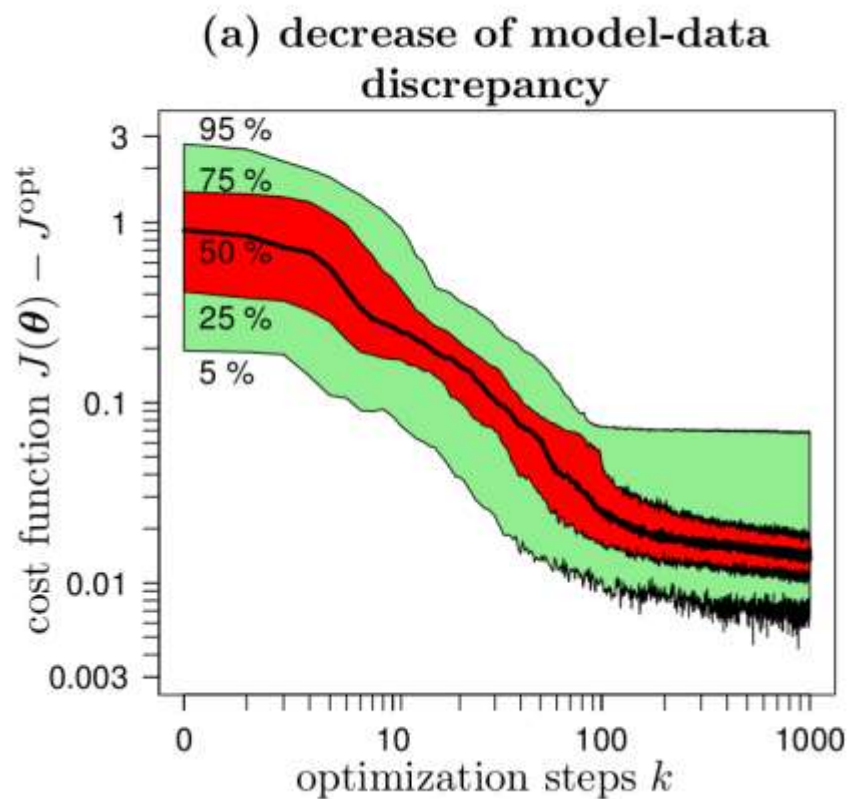
# J Gradient estimation

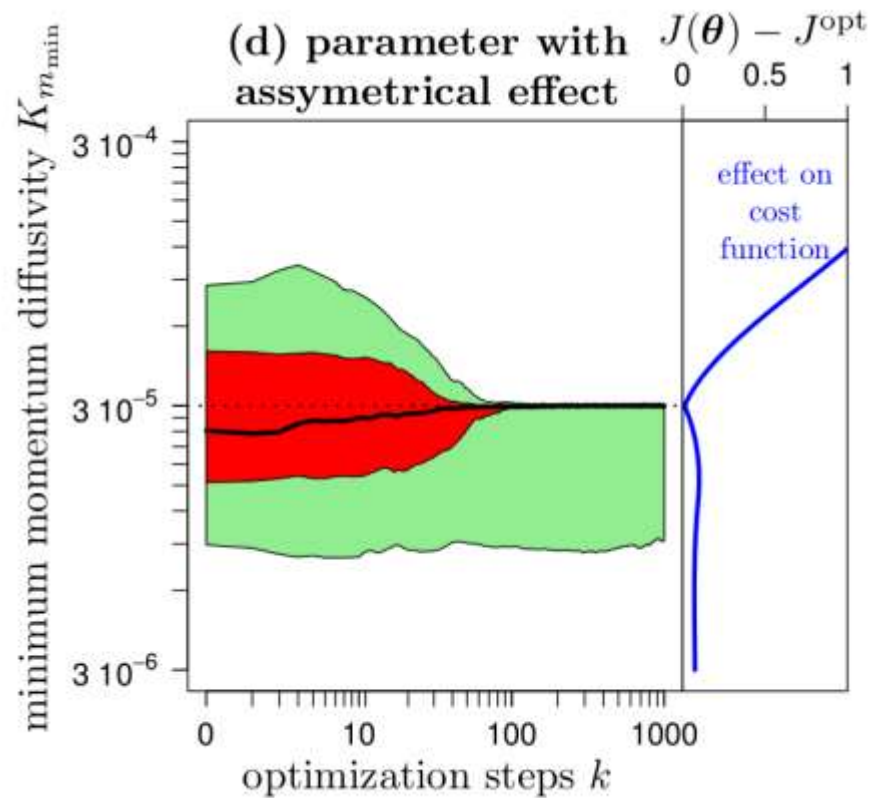
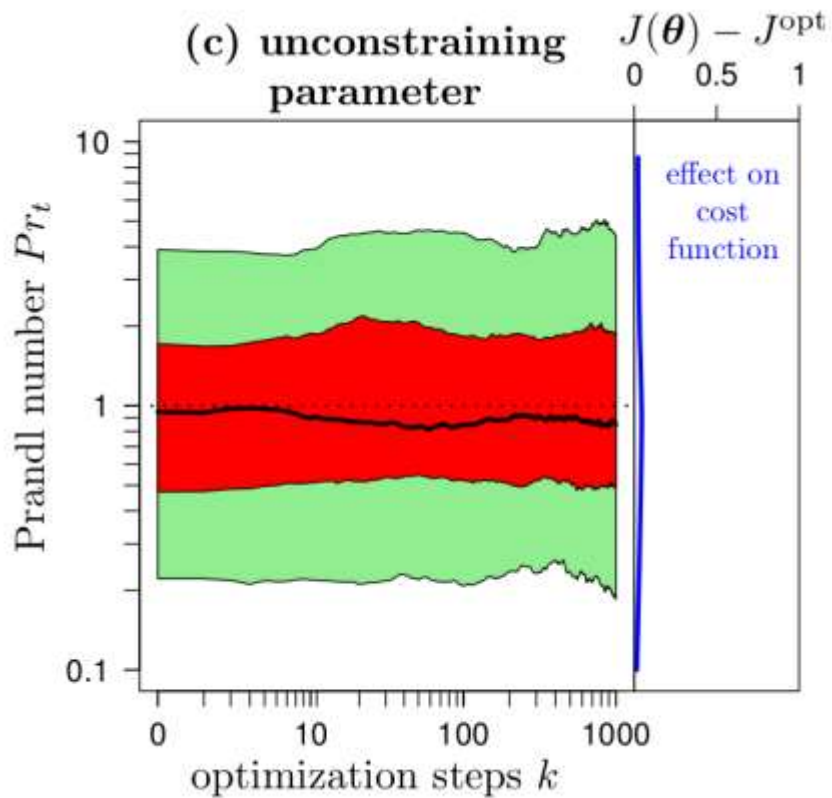
Classical : 1  
Parameter  
at a time

$$\nabla J(\boldsymbol{\theta}^k) = \begin{pmatrix} \frac{J(\boldsymbol{\theta}^{(k)} + \delta\boldsymbol{\theta}_1^{(k)}) - J(\boldsymbol{\theta}^{(k)} - \delta\boldsymbol{\theta}_1^{(k)})}{2c^{(k)}} \\ \vdots \\ \frac{J(\boldsymbol{\theta}^{(k)} + \delta\boldsymbol{\theta}_i^{(k)}) - J(\boldsymbol{\theta}^{(k)} - \delta\boldsymbol{\theta}_i^{(k)})}{2c^{(k)}} \\ \vdots \\ \frac{J(\boldsymbol{\theta}^{(k)} + \delta\boldsymbol{\theta}_p^{(k)}) - J(\boldsymbol{\theta}^{(k)} - \delta\boldsymbol{\theta}_p^{(k)})}{2c^{(k)}} \end{pmatrix}, \quad \delta\boldsymbol{\theta}_i^{(k)} = c^{(k)} \begin{pmatrix} 0 \\ \vdots \\ 0 \\ 1 \\ 0 \\ \vdots \\ 0 \end{pmatrix} \quad (4)$$

SPSA  
simultaneous  
Perturbations of  
All parameters

$$\nabla J(\boldsymbol{\theta}^k) = \begin{pmatrix} \frac{J(\boldsymbol{\theta}^{(k)} + \delta\boldsymbol{\theta}^{(k)}) - J(\boldsymbol{\theta}^{(k)} - \delta\boldsymbol{\theta}^{(k)})}{2c^{(k)}\Delta_1^{(k)}} \\ \vdots \\ \frac{J(\boldsymbol{\theta}^{(k)} + \delta\boldsymbol{\theta}^{(k)}) - J(\boldsymbol{\theta}^{(k)} - \delta\boldsymbol{\theta}^{(k)})}{2c^{(k)}\Delta_i^{(k)}} \\ \vdots \\ \frac{J(\boldsymbol{\theta}^{(k)} + \delta\boldsymbol{\theta}^{(k)}) - J(\boldsymbol{\theta}^{(k)} - \delta\boldsymbol{\theta}^{(k)})}{2c^{(k)}\Delta_p^{(k)}} \end{pmatrix}, \quad \delta\boldsymbol{\theta}^{(k)} = c^{(k)} \begin{pmatrix} \Delta_1^{(k)} \\ \vdots \\ \Delta_i^{(k)} \\ \vdots \\ \Delta_p^{(k)} \end{pmatrix} \quad (5)$$





# Comments and perspectives

- Example of use of SPSA method for a turbulent closure scheme embedded in a one-dimensional vertical model of the ocean.

- Parameters that constrain model predictions are estimated with a high accuracy.

- Some other parameters are well-estimated on average, but with less accuracy(The same as other methods)

- Results are obtained at a relatively low numerical cost.

- Allows to optimize models without an adjoint model costly to derive.

- Method fast enough to allow repetitions, to perform a sensitivity analysis

- Easy to change the optimization problem to solve (model, cost function, available data)

- Possibility to use for boundary conditions fitting or in coupled hydrodynamic-biogeochemical models

# Persistence extremal index method

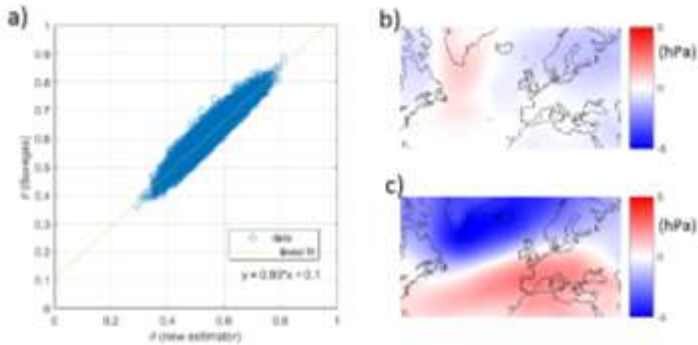


FIGURE 3. a) Scatter plot of  $\hat{\theta}_{Sve}$  (the Süveges estimator) vs  $\hat{\theta}_S$  (the new estimator introduced in this work). Average map of the 5% sea-level pressure patterns such that the residual between  $\hat{\theta}_{Sve}$  and  $\hat{\theta}_S$  are smaller than the 5% percentile (b) or larger (c) than the 95% percentile, for both taking as a threshold the 0.99-quantile of the observable distribution.

Caby, Faranda, Vaienti, Yiu, 2019

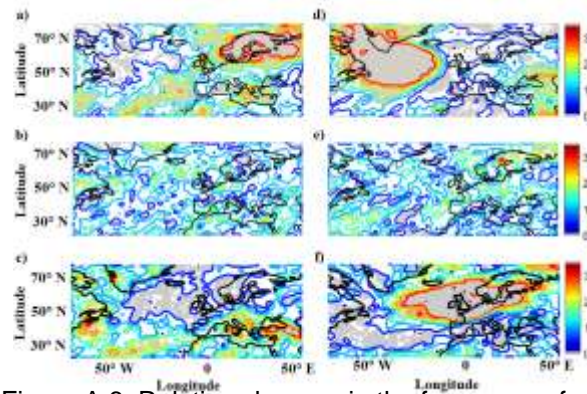
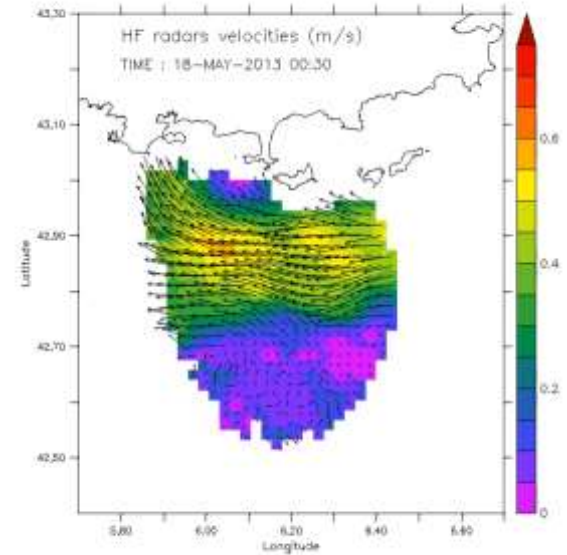
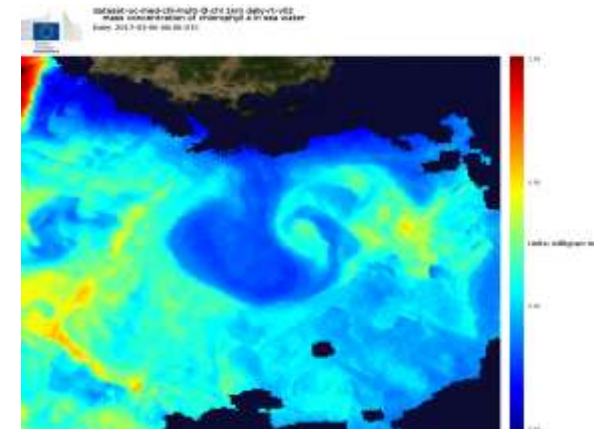


Figure A.6: Relative changes in the frequency of a), d) extreme cold; b), e) extreme wet and c), f) extreme 10m wind events for days with instantaneous dimension beyond the a-c) 0.98 and d-f) 0.02 quantiles of  $d$  in the ERA-Interim data. Contours start at 0, with an interval of 0.5; the grey shading shows statistically significant changes. The maps in this gure are generated by MATLAB R2013a.

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# Conclusions

- 3D observations of the marine surface layer in microtidal sea have been started (2DH HF radars + 1V ADP/CTD profilers)
- Sensitivity of the surface mixing layer to eddy viscosity as function of 3D space and time has been investigated (still in a very limited number of situations)
- A fast method for Identification of parameters of turbulent closure models (TKE, KPP, etc) has been proposed (tests in progress)
- A data analysis approach based on dynamical systems has been proposed for sparse data sets to classify events (from rare to extreme) and provide statistics (persistence)
- Ekman model needs to be revisited for high resolution modeling (surface and internal waves, Stokes drift, Langmuir circulations, horizontal variations)



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